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# High order finite difference schemes for the solution of second order initial value problems

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*Abstract:* The numerical solution of second order ordinary differential equations with initial conditions is here approached by approximating each derivative by means of a set of finite difference schemes of high order. The stability properties of the obtained methods are discussed. Some numerical tests, reported to emphasize pros and cons of the approach, motivate possible choices on the use of these formulae.

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# 1 Introduction

The study of second order differential equations

 $\mathcal{F}(t, y, y', y'') = 0$ 

has a huge bibliography covering several applicative fields, from chemistry to physics and engineering. Even if any high order ODE may be recast as a first order one, this transformation increases the size of the original problem and should make its numerical solution more complicated since it requires the computation of both solution and derivatives (which have different slopes) at the same time.

The most interesting and studied second order problems are two-point boundary value problems (see [7] and the reference therein). Among these, two-point singular perturbation problems (see [11])

$$\epsilon y^{\prime\prime} = f(t, y, y^{\prime}), \qquad 0 < \epsilon \ll 1,$$

have a great appeal since they are stiff, and hence several numerical techniques have been considered for their solution. Among these we recall, for example, collocation methods (see [6]), largely used in the codes.

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Most of the initial value problems arise from celestial mechanics and lack of the first derivative term. For such problems (called conservative) ad hoc methods have been developed that preserve some properties of the solution [1, 14]. In this paper we are rather interested in initial value problems with nonnull derivative terms since they are not integrated with classical linear multistep formulae. A wide class of such problems arises from singular problems (not defined at some points of the domain, see, for example, [13]) that however will not be considered in this paper. Moreover, some of these are involved in the solution of the nonlinear Schrödinger equation which forms the envelope equation for many physical processes and also for the transverse modulation of a water wave [9, 10].

The idea carried on through this paper is largely used to solve partial differential equations on regular domains. In fact, when it is possible to subdivide the domain with regular grids, each derivative term can be separately approximated. The main gap of this approach is the order of the obtained approximation which is at most 2.

In [4] it is suggested how to overcome this problem for BVPs. As a matter of fact, by using the typical approach of BVMs [8] (initial, main and final formulae), it is possible to obtain stable formulae of arbitrary high order. In [5] a generalization of the first order upwind method has been derived for scalar singular perturbation problems. A code based on these formulae is proposed in [2, 3].

Here we apply the same idea to general second order initial value problems. The paper is organized as follows: in the next section we introduce high order finite differences to approximate each derivative of the second order problem. Section 3 concerns with the additional schemes that must be considered in order to use the known value of the first derivative at the initial point. Finally, the last section is devoted to various test examples that are solved by means of both constant and variable meshes.

## 2 High order finite difference approximations

Let us analyze the following second-order initial value problem:

$$\begin{cases} f(t, y, y', y'') = 0, \\ y(t_0) = y_0, \quad y'(t_0) = y'_0, \end{cases}$$
(1)

where  $y_0$  and  $y'_0$  are known values. Let us assume that f is a Lipschitz continuous function in order there exists a unique solution y(t) of the above problem.

Let

$$t_0 < t_1 < \dots < t_n \tag{2}$$

be a discretization covering all the time-interval or a part of it. The idea proposed in [2, 4, 5] for the solution of BVPs is that of computing the numerical solution  $Y = (y_0, y_1, \ldots, y_n)^T$  of (1) at the meshpoints (2) by approximating  $y'(t_i)$  and  $y''(t_i)$ , for  $i = 1, \ldots, n-1$ , by means of appropriate finite difference schemes

$$y^{(\nu)}(t_i) \approx y_i^{(\nu)} = \frac{1}{h_i^{\nu}} \sum_{j=-s}^{k-s} \alpha_{j+s}^{(\nu)} y_{i+j}, \qquad \nu = 1, 2,$$
(3)

where  $h_i = t_i - t_{i-1}$  and the coefficients  $\alpha_0^{(\nu)}, \ldots, \alpha_k^{(\nu)}$  are computed such that the formulae have maximum order. In (3) the index k depends on  $\nu$  and the order of the formula (an order p approximation for  $y^{(\nu)}(t_i)$  is in general defined on  $p + \nu$  points),  $0 \le s \le k$  and the coefficients depend on k, s, and  $\nu$ .

For Boundary Value Problems, this kind of approach uses variable meshes to discretize the whole time interval. Here, it is preferable to discretize recursively small parts of it by using (for simplicity) constant stepsize inside each subinterval. For this reason, the coefficients of the methods (computed by solving Vandermonde linear systems with integer coefficients) are exactly derived.

With respect to the formulae suggested in [2, 4, 5] we have to note that the initial condition  $y'(t_0)$  in (1) is not used in (3) which only works with the values  $y_i \approx y(t_i)$ . Possible approaches to make use of  $y'(t_0)$  will be considered in the next section. For the moment, we recall that the methods approximating the derivatives are based on the idea of Boundary Value Methods [8]. For each derivative we fix the order and derive the set of finite difference schemes (3) by changing conveniently the number s and k - s of initial and final conditions, respectively. Among these formulae, we emphasize the main scheme which will be used when possible on the points of the mesh (2). The other formulae (or some of them) will be used once in the extreme points of the mesh. For example, to approximate  $y'(t_n)$  and  $y'(t_1)$  it is necessary to use a final method with only initial conditions and an initial method with at most 1 initial condition, respectively. In vector form the overall approximations for the  $\nu$ -th derivative can be cast as

$$Y^{(\nu)} = \frac{1}{h^{\nu}} A_{\nu} \cdot Y, \qquad \nu = 1, 2,$$

where  $A_{\nu}$  is a  $(n-1) \times (n+1)$  coefficient matrix, whereas  $\overline{Y}$ , containing the n-1 unknowns of Y, is the solution of the nonlinear system of equations

$$f(\overline{Y}, Y^{(1)}, Y^{(2)}) = 0.$$
(4)

In the linear case, (4) is a linear system

$$M \cdot \overline{Y} = b \tag{5}$$

with the coefficient matrix M having essentially a band structure.

We examine only main schemes with approximatively the same number of initial and final conditions. According to several previous papers (see, for example, [4] and the references therein), we call extended central (EC) differences those having the same number of initial and final conditions. The coefficients of EC schemes are symmetric for the second derivative and skew-symmetric for the first derivative. On the contrary, if s again denotes the number of initial conditions, we call generalized backward (GB) and generalized forward (GF) differences those having s-1 or s-2and s+1 or s+2 final conditions, respectively, depending on the order of the method. In the following, a subscript after the acronym suggests the derivative to which the scheme is applied. For the second derivative, we consider three possible choices depending on the overall order p. For even orders, we use a symmetric scheme EC<sub>2</sub> (defined for k = p and  $s = \frac{k}{2}$ ) while for odd orders we choose between generalized forward  $GF_2$  or backward differences  $GB_2$  (defined for k = p + 1and  $s = \frac{k}{2} - 1$  or  $s = \frac{k}{2} + 1$ , respectively). For the first derivative, we have k = p and s may be chosen between  $\frac{k-1}{2}$  and  $\frac{k+1}{2}$  if k is odd, and among  $\frac{k}{2} - 1, \frac{k}{2}, \frac{k}{2} + 1$  if k is even. These formulae will be called GF<sub>1</sub>, EC<sub>1</sub> and GB<sub>1</sub> according to what said previously. The combination of such formulae gives rise to 7 couple of main schemes (it is not possible to define symmetric schemes of odd order):  $EC_2EC_1$ ,  $EC_2GF_1$  and  $EC_2GB_1$  of even order which were already used for BVPs (see [2, 4, 5] where it is important to consider a symmetric approximation for the second derivative, and  $GB_2GB_1$ ,  $GB_2GF_1$ ,  $GF_2GB_1$  and  $GF_2GF_1$  of odd order. In the section devoted to the numerical tests, we only consider couple of methods with the same approximation for the derivatives, namely  $EC_2EC_1$ ,  $GB_2GB_1$ , and  $GF_2GF_1$ .

As an example, the following are main schemes of order 5 and 6 for the approximation of y'and y''. The coefficients of the GB<sub>2</sub> (GB<sub>1</sub>) schemes are symmetric (skew-symmetric) with respect to those of the  $GF_2$  ( $GF_1$ ) schemes.

Order 5

$$GF_{2}: \qquad h^{2} y''(t_{i}) \approx -\frac{13}{180}y_{i-2} + \frac{19}{15}y_{i-1} - \frac{7}{3}y_{i} + \frac{10}{9}y_{i+1} + \frac{1}{12}y_{i+2} - \frac{1}{15}y_{i+3} + \frac{1}{90}y_{i+4}$$

$$GF_{1}: \qquad h y'(t_{i}) \approx \frac{1}{20}y_{i-2} - \frac{1}{2}y_{i-1} - \frac{1}{3}y_{i} + y_{i+1} - \frac{1}{4}y_{i+2} + \frac{1}{30}y_{i+3}$$

Order 6

EC<sub>2</sub>: 
$$h^2 y''(t_i) \approx \frac{1}{90} y_{i-3} - \frac{3}{20} y_{i-2} + \frac{3}{2} y_{i-1} - \frac{49}{18} y_i + \frac{3}{2} y_{i+1} - \frac{3}{20} y_{i+2} + \frac{1}{90} y_{i+3}$$

EC<sub>1</sub>: 
$$h y'(t_i) \approx -\frac{1}{60}y_{i-3} + \frac{1}{20}y_{i-2} - \frac{1}{4}y_{i-1} + \frac{1}{4}y_{i+1} - \frac{1}{20}y_{i+2} + \frac{1}{60}y_{i+3}$$
  
GF<sub>1</sub>:  $h y'(t_i) \approx \frac{1}{30}y_{i-2} - \frac{2}{5}y_{i-1} - \frac{7}{12}y_i + \frac{4}{3}y_{i+1} - \frac{1}{2}y_{i+2} + \frac{2}{15}y_{i+3} - \frac{1}{60}y_{i+4}$ 

To investigate the stability properties of the main schemes for the two derivatives, let us analyze their behavior on scalar linear problems of the form

$$y'' + \gamma y' + \mu y = 0, \tag{6}$$

where  $\gamma$  and  $\mu$  are real numbers independent of t. If associated to initial conditions, (6) is well conditioned only when  $\gamma$  and  $\mu$  are non negative values. In particular, the general solution of (6),

$$y(t) = c_1 e^{r_1 t} + c_2 e^{r_2 t}$$

where  $c_1$  and  $c_2$  depend on the initial conditions and  $r_1$  and  $r_2$  are roots (supposed distinct) of the equation  $r^2 + \gamma r + \mu = 0$ , is monotone decreasing when  $\gamma > 0$  and bounded for  $\gamma = 0$ . Depending on the initial conditions, y(t) may be strictly positive on all the time interval.

Supposing for the moment that the size n of the grid is large, then the effect of the additional methods on the solution may be considered negligible. Therefore, it is sufficient to study the roots of the characteristic polynomial

$$\pi(z) = \rho(z) + h\gamma\sigma(z) + h^2\mu z^{\bar{s}}, \qquad \bar{s} = \max(s_1, s_2)$$

where  $\rho$  and  $\sigma$  are the polynomials associated to the main schemes discretizing, respectively, the second and the first derivative term in (6), and  $s_{\nu}$ ,  $\nu = 1, 2$ , is the value of s in (3) associated to the  $\nu$ -th derivative. We require that the number of upper off-diagonals of the coefficient matrix in (5) matches the number of roots of  $\pi$  outside the open unit disk [8]. Since  $\gamma$  and  $\mu$  are real numbers, essentially this means that in the quarter of the plane with  $h\gamma \geq 0$  and  $h^2\mu \geq 0$  we have to draw the boundary locus defined by the the straight lines  $\pi(1) = 0$  and  $\pi(-1) = 0$ , and by the curve  $\pi(z) = 0$  with |z| = 1 and  $\operatorname{Im}(z) \neq 0$ . Since z = 1 is always a root of both  $\rho$  and  $\sigma$ , the first straight line coincides with the abscissa  $h^2\mu = 0$ . The condition  $\pi(-1) = 0$  corresponds to the straight line  $\sigma_1 h\gamma + h^2 \mu \leq \rho_1$ , where  $\sigma_1$  and  $\rho_1$  are summarized in Tables 1 and 2 for different methods and orders. Since  $\rho_1 > 0$ , the straight lines corresponding to GB<sub>1</sub>, GF<sub>1</sub> and EC<sub>1</sub> schemes are decreasing ( $\sigma_1 > 0$ ), increasing ( $\sigma_1 < 0$ ) and parallel to the  $h\gamma$ -axis ( $\sigma_1 = 0$ ), respectively. Hence, the use of GF<sub>1</sub> schemes give rise to the largest stability domain. Finally, the curve corresponding to the complex values of z of unitary modulus starts from the origin and it is quite near to the  $h^2\mu$ -axis (it coincides with the segment  $0 \leq h^2\mu \leq \rho_1$  in case of EC<sub>1</sub> schemes).

We observe that any combination of formulae does not give stable methods for every value of h (following [8] we say that there is no  $A_{s,k-s}$ -stable method). As an example, we plot in Figure 1 the stability domains for the GF<sub>2</sub>GF<sub>1</sub> and GB<sub>2</sub>GB<sub>1</sub> schemes of order 5 and 7. We note that the higher order methods have a larger stability domain.

Table 1: Coefficients  $\sigma_1$  and  $\rho_1$  of the straight line  $\sigma_1 h \gamma + h^2 \mu = \rho_1$  corresponding to  $\pi(-1) = 0$ . Even order approximations.

|                 |            |      |        | order    |          |
|-----------------|------------|------|--------|----------|----------|
|                 |            | 4    | 6      | 8        | 10       |
| $EC_2$          | $\rho_1$   | 16/3 | 272/45 | 2048/315 | 512/75   |
| $\mathrm{GF}_1$ | $\sigma_1$ | -8/3 | -32/15 | -64/35   | -512/315 |
| $GB_1$          | $\sigma_1$ | 8/3  | 32/15  | 64/35    | 512/315  |
| $\mathrm{EC}_1$ | $\sigma_1$ | 0    | 0      | 0        | 0        |

Table 2: Coefficients  $\sigma_1$  and  $\rho_1$  of the straight line  $\sigma_1 h \gamma + h^2 \mu = \rho_1$  corresponding to  $\pi(-1) = 0$ . Odd order approximations.

|                               |            | order |        |        |           |  |  |
|-------------------------------|------------|-------|--------|--------|-----------|--|--|
|                               |            | 3     | 5      | 7      | 9         |  |  |
| $\mathrm{GF}_2/\mathrm{GB}_2$ | $\rho_1$   | 8/3   | 208/45 | 352/63 | 9278/1575 |  |  |
| $GF_1$                        | $\sigma_1$ | -4/3  | -16/15 | -32/35 | -256/315  |  |  |
| $GB_1$                        | $\sigma_1$ | 4/3   | 16/15  | 32/35  | 256/315   |  |  |

The case  $\gamma = 0$  is not efficiently solved by this approach when the time interval is very large. In fact, as already known, second order IVPs y'' = f(t, y) are properly solved by symmetric linear multistep methods that do not fall in this class of methods.

## 3 Additional formulae

From the number of roots greater than 1 in modulus inside the boundary locus we obtain that, despite the continuous problem has initial conditions, each main scheme (3) requires s - 1 initial and k - s - 1 final formulae. Hence, for example, the EC schemes must always be joined to the same number of initial and final formulae.

This section just concerns with the additional schemes we have to use in order to approximate y' and y'' at both the extreme points of (2). In general we consider formulae in the family (3) with a reduced number of initial or final conditions. Anyway, for second order initial value problems (1), the function f is not approximated at  $t_0$  and, hence, the initial value  $y'(t_0)$  is not used. Then, we may follow two strategies: the first one is to consider a formula approximating  $y'(t_0)$  as an additional equation, thus obtaining the following system

$$\begin{cases} y_0 \text{ given,} \\ \frac{1}{h} \sum_{j=0}^k \alpha_j y_j = y'_0, \\ f(t_i, y_i, y'_i, y''_i) = 0, \quad \text{for } i = 1, \dots, n-1, \end{cases}$$
(7)

which provides a unique solution  $Y = (y_0, y_1, \dots, y_n)^T$  of the discrete problem.

The second strategy is based on the new initial formulae

$$y^{(\nu)}(t_i) \approx \frac{1}{h^{\nu}} \left( \bar{\alpha}_0^{(\nu,i)} h y_0' + \sum_{j=1}^k \alpha_j^{(\nu,i)} y_{j-1} \right), \qquad \nu = 1, 2,$$
(8)



Figure 1: Stability regions for the  $GF_2GF_1$  (left) and  $GB_2GB_1$  (right) schemes of order 5 and 7.

that use the prescribed value  $y'_0$ . Then  $Y = (y'_0, y_0, y_1, \dots, y_n)^T$  is computed by means of

$$\begin{cases} y_0, y'_0 \text{ given,} \\ f(t_i, y_i, y'_i, y''_i) = 0, \quad \text{for } i = 0, \dots, n-1. \end{cases}$$
(9)

Both the approaches are applicable to the first block of approximations, corresponding to the initial subinterval. If  $t_n$  is not the end-point of the time interval (we need other blocks to cover the time domain), from the second block on we could use the last two points as known initial values of the new block and formulae (3) to uniquely compute  $Y = (y_{-1}, y_0, y_1, \ldots, y_n)^T$  from

$$\begin{cases} y_0, y_{-1} \text{ given,} \\ f(t_i, y_i, y'_i, y''_i) = 0, \quad \text{for } i = 0, \dots, n-1. \end{cases}$$
(10)

In case the stepsize is changed, the initial value  $y_{-1}$  is computed by means of interpolation techniques from the points in the previous block. As an alternative, it is possible to define a formula analogous to that in (7) to compute an approximation to  $y'(t_n)$  and then use the same set of formulae considered for the first block.

Concerning the approach in (9), for symmetry reason it is more convenient to set  $Y = (y'_0, y_0, y_1, \ldots, y_n, y'_n)^T$  and use (9) (for  $i = 0, \ldots, n$ ) with schemes analogous to (8),

$$y^{(\nu)}(t_{n-i}) \approx \frac{(-1)^{\nu}}{h^{\nu}} \left( -\bar{\alpha}_0^{(\nu,i)} h y'_n + \sum_{j=1}^k \alpha_j^{(\nu,i)} y_{n-j+1} \right), \qquad \nu = 1, 2,$$
(11)

as final formulae. We observe that the coefficients in (11) for  $y^{(\nu)}(t_{n-i})$  are just the same as those in (8) for  $y^{(\nu)}(t_i)$ .

From a numerical point of view, the last formula, even if it is described in compact form and it is applicable to any block of the time interval, contains values of y and y' that could be different in magnitude. Anyway, the numerical tests show that this approach gives the most accurate results. The idea of neglecting the value of the derivative after the first block seems to be more natural for this kind of approach but it requires interpolation formulae that could be ill-conditioned if the order is high since the used stepsize inside each block is constant. Possibly, a variable stepsize inside each block could be advantageous, but we shall not consider this issue here.

As an example, the following are initial formulae in (8) of order 5 and 6 (we recall that  $y'(t_0) = y'_0$ ).

Order 5  

$$h^2 y''(t_0) \approx -\frac{137}{30} hy'_0 - \frac{12019}{1800} y_0 + 10y_1 - 5y_2 + \frac{20}{9} y_3 - \frac{5}{8} y_4 + \frac{2}{25} y_5$$
  
 $h^2 y''(t_1) \approx \frac{13}{30} hy'_0 + \frac{3281}{1800} y_0 - \frac{41}{12} y_1 + \frac{11}{6} y_2 - \frac{5}{18} y_3 + \frac{1}{24} y_4 - \frac{1}{300} y_5$   
 $h y'(t_1) \approx -\frac{1}{4} hy'_0 - \frac{37}{48} y_0 + \frac{1}{6} y_1 + \frac{3}{4} y_2 - \frac{1}{6} y_3 + \frac{1}{48} y_4$ 

Order 6

$$\begin{split} h^2 \ y''(t_0) &\approx -\frac{49}{10} hy_0' - \frac{13489}{1800} y_0 + 12y_1 - \frac{15}{2} y_2 + \frac{40}{9} y_3 - \frac{15}{8} y_4 + \frac{12}{25} y_5 - \frac{1}{18} y_6 \\ h^2 \ y''(t_1) &\approx \frac{77}{180} hy_0' + \frac{2171}{1200} y_0 - \frac{203}{60} y_1 + \frac{43}{24} y_2 - \frac{13}{54} y_3 + \frac{1}{48} y_4 + \frac{1}{300} y_5 - \frac{1}{1080} y_6 \\ h \ y'(t_1) &\approx -\frac{1}{5} hy_0' - \frac{197}{300} y_0 - \frac{1}{12} y_1 + y_2 - \frac{1}{3} y_3 + \frac{1}{12} y_4 - \frac{1}{100} y_5 \end{split}$$

#### 4 Numerical examples

In this section we compare both the numerical schemes described in Section 2 and the possible choices for the additional formulae described in Section 3 on two linear and one nonlinear initial value problems. In our numerical experiments we have used blocks with p + 4 equidistant points, where the order p ranges from 3 to 10.

For all the examples we have first considered a constant stepsize implementation (see Tables 3, 4, and 5) in order to estimate the order of convergence and to compare the methods. Then, we have solved each problem by means of a simple variable stepsize strategy (see Tables 6, 7, 8, and 9) with initial stepsize  $h_0 = 8 \cdot 10^{-2}$  and exit tolerance  $tol = 10^{-8}$ . As usual for this kind of solvers (see [2, 3]), the method of order p + 2 allows us to estimate the error for the method of order p and a new steplength for the successive block by means the formula

$$h_{new} = 0.9 \left(\frac{tol}{err}\right)^{1/(p+1)} h_{old}.$$

However, in the tables we list the actual absolute error.

We focus our attention on three methods which differ each other for the considered additional (initial/final) methods. The first two methods use (7) for the first block. Then the first method (Method 1) computes an approximation for  $y'(t_{n-1})$  (since the error constant for this formula is much lower than the analogous at  $t_n$ , the approximation  $y_n$  at  $t_n$  is discarded) and iterates on the subsequent blocks. The second method (Method 2) uses  $y_n$  and  $y_{n-1}$  as initial points in order to apply (10) to the subsequent blocks. Since this approach should require a very carefully interpolation technique, we have not considered it with variable stepsize. The third method (Method 3) uses (9), the initial formulae (8) and the final formulae (11).

Problem 1. The first linear problem,

$$y''(t) + y'(t) = 0, \qquad t \in [0, 40],$$

| [             | Main                            |       | Method1 Method2      |                |                      |                | Met      | hod3           |
|---------------|---------------------------------|-------|----------------------|----------------|----------------------|----------------|----------|----------------|
|               | Scheme                          | Order | Error                | t: y(t) < 0    | Error                | t: y(t) < 0    | Error    | t: y(t) < 0    |
|               | CF-CF.                          | 3     | 4.650.05             |                | 3,000,06             | 12.06          | 3 400 06 | ÷ • 9(*)   • • |
| ts            | $GB_2GP_1$                      | 3     | 4.03e-05<br>4.49e-05 |                | 3.90e-00<br>8.40e-06 | 12.90<br>11.76 | 6.21e-06 | 12.00          |
| in            | $EC_2EC_1$                      | 4     | 3 31e-05             | 10.32          | 1.89e-05             | 10.88          | 2.88e-07 | 16.24          |
| po            | GE <sub>2</sub> GE <sub>1</sub> | 5     | 2.50e-08             | 10.02          | 6.70e-08             | 16.56          | 9.86e-09 | 18.48          |
| 00            | $GB_2GP_1$                      | 5     | 2.50e-08             |                | 2 35e-08             | 10.50<br>17.60 | 1.65e-08 | 10.40          |
| 5             | $EC_2EC_1$                      | 6     | 1.44e-07             | 15 76          | 2.55e-08             | 16.24          | 3 57e-09 |                |
| <u>م</u>      | GE <sub>2</sub> GE <sub>1</sub> | 7     | $1.93e_{-10}$        | 23.92          | 2.68e-10             | 22.08          | 1.88e-11 |                |
| 0             | GB <sub>2</sub> GB <sub>4</sub> | 7     | 1.23e-10<br>1.23e-10 | 23.92          | 2.03e-10<br>2.53e-10 | 22.00<br>22.16 | 1.45e-11 | 24.96          |
|               | EC <sub>2</sub> EC <sub>4</sub> | 8     | 7.05e-10             | 25.32<br>21.12 | 2.35e-10             | 22.10<br>21.52 | 0.04e-12 | 24.30          |
| ×             | GE <sub>2</sub> GE <sub>1</sub> | 9     | 1.05e-10<br>1.15e-12 | 21.12<br>27.76 | 1.50e-10             | 21.02<br>27.20 | 2.04e-12 | 32 56          |
| 11            | $GB_2GP_1$                      | 9     | 6 31e-13             | 28.40          | $1.37e_{-12}$        | 27.36          | 5.28e-14 | 02.00          |
| $^{\prime}$   | $EC_2EC_1$                      | 10    | 3.57e-12             | 26.40<br>26.40 | $2.60e_{-12}$        | 21.00<br>26.72 | 3 36e-14 |                |
|               | DO2DO1                          | 10    | 3.576-12             | 20.40          | 2.000-12             | 20.12          | 5.506-14 |                |
| ts            | $GF_2GF_1$                      | 3     | 1.54e-05             |                | 1.73e-07             | 14.04          | 5.13e-07 | 14.00          |
| in            | $GB_2GB_1$                      | 3     | 1.51e-05             | 10.40          | 8.06e-07             | 14.04          | 6.89e-07 | 14.20          |
| po            | $EC_2EC_1$                      | 4     | 3.94e-06             | 12.48          | 1.72e-06             | 13.28          | 1.78e-08 | 18.96          |
| 00            | $GF_2GF_1$                      | 5     | 5.36e-09             |                | 1.57e-09             | 20.28          | 3.64e-10 | 21.76          |
| 10            | $GB_2GB_1$                      | 5     | 6.90e-09             | 10.00          | 3.31e-10             | 21.96          | 4.69e-10 |                |
| ~             | $EC_2EC_1$                      | 6     | 4.36e-09             | 19.28          | 2.06e-09             | 20.04          | 5.65e-11 |                |
| 1             | $GF_2GF_1$                      | 7     | 2.82e-12             |                | 1.40e-12             | 27.32          | 1.62e-13 | 00.14          |
| 10            | $GB_2GB_1$                      | 7     | 3.02e-12             | 22.00          | 1.43e-12             | 27.28          | 8.20e-14 | 30.16          |
| स             | $EC_2EC_1$                      | 8     | 5.24e-12             | 26.00          | 2.71e-12             | 26.64          | 6.20e-14 |                |
| Î             | $GF_2GF_1$                      | 9     | 1.90e-13             | 00.00          | 6.79e-14             |                | 7.33e-15 |                |
| - 4           | $GB_2GB_1$                      | 9     | 4.30e-13             | 28.60          | 3.75e-13             | 00.00          | 1.48e-14 | 00 50          |
|               | $EC_2EC_1$                      | 10    | 2.30e-13             |                | 1.17e-13             | 30.20          | 5.53e-14 | 30.56          |
| $\mathbf{ts}$ | $GF_2GF_1$                      | 3     | 4.31e-06             |                | 4.92e-08             |                | 6.96e-08 |                |
| in            | $GB_2GB_1$                      | 3     | 4.27e-06             |                | 8.36e-08             | 16.30          | 8.06e-08 | 16.34          |
| bc            | $EC_2EC_1$                      | 4     | 4.79e-07             | 14.56          | 1.69e-07             | 15.60          | 1.11e-09 | 21.74          |
| 0             | $GF_2GF_1$                      | 5     | 4.66e-10             |                | 3.90e-11             | 23.98          | 1.21e-11 | 25.14          |
| 00            | $GB_2GB_1$                      | 5     | 5.14e-10             |                | 3.72e-12             | 27.56          | 1.41e-11 |                |
|               | $EC_2EC_1$                      | 6     | 1.34e-10             | 22.74          | 4.97e-11             | 23.74          | 8.78e-13 |                |
| -2            | $GF_2GF_1$                      | 7     | 3.53e-13             |                | 9.57e-14             |                | 2.43e-13 |                |
| 10            | $GB_2GB_1$                      | 7     | 3.20e-13             | 28.80          | 2.78e-13             |                | 1.67e-13 |                |
|               | $EC_2EC_1$                      | 8     | 3.74e-14             |                | 1.69e-13             | 29.42          | 1.40e-13 |                |
|               | $GF_2GF_1$                      | 9     | 3.27e-12             |                | 1.40e-12             |                | 9.58e-14 | 29.98          |
|               | $GB_2GB_1$                      | 9     | 7.33e-13             | 27.96          | 3.38e-13             |                | 2.34e-14 | 31.70          |
| (             | $EC_2EC_1$                      | 10    | 1.27e-12             |                | 1.26e-12             |                | 1.41e-13 | 29.60          |
| ŝ             | $GF_2GF_1$                      | 3     | 1.13e-06             |                | 8.23e-09             |                | 9.04e-09 |                |
| int           | $GB_2GB_1$                      | 3     | 1.13e-06             |                | 9.32e-09             | 18.50          | 9.73e-09 | 18.45          |
| od            | $EC_2EC_1$                      | 4     | 5.90e-08             | 16.65          | 1.81e-08             | 17.83          | 6.99e-11 | 24.58          |
| 0             | $GF_2GF_1$                      | 5     | 3.36e-11             |                | 9.73e-13             |                | 3.17e-13 |                |
| 00            | $GB_2GB_1$                      | 5     | 3.46e-11             |                | 1.45e-12             |                | 1.10e-12 |                |
| 4             | $EC_2EC_1$                      | 6     | 4.64e-12             | 26.10          | 1.05e-12             | 27.58          | 3.03e-13 | 28.83          |
| 5             | $GF_2GF_1$                      | 7     | 8.91e-13             | 27.75          | 2.93e-13             | 28.89          | 6.06e-13 |                |
| .01           | $GB_2GB_1$                      | 7     | 1.14e-12             | 27.51          | 4.40e-13             | 28.46          | 7.39e-13 |                |
|               | $EC_2EC_1$                      | 8     | 4.22e-13             | 28.57          | 3.62e-13             | 28.65          | 7.77e-13 |                |
|               | $GF_2GF_1$                      | 9     | 1.13e-11             |                | 3.48e-12             |                | 4.14e-14 | 33.80          |
|               | $GB_2GB_1$                      | 9     | 1.83e-12             |                | 1.61e-12             | 27.64          | 2.39e-13 | 29.07          |
| ŀ.            | $EC_2EC_1$                      | 10    | 7.58e-12             |                | 4.30e-12             |                | 9.27e-13 | 27.71          |

Table 3: Numerical results for Test problem 1 with y(0) = 1, constant stepsize.

|                            | Main                            |             | 1                    | Error    |          |
|----------------------------|---------------------------------|-------------|----------------------|----------|----------|
|                            | Scheme                          | Order       | Method1              | Method2  | Method3  |
|                            | CF <sub>2</sub> CF <sub>4</sub> | 3           | 7.630-03             | 1 730-03 | 2 000-03 |
| $_{\rm its}$               | $GB_2GB_1$                      | 3           | 7.31e-04             | 6.64e-03 | 3.30e-03 |
| nic                        | EC <sub>2</sub> EC <sub>1</sub> | 4           | 2.46e-03             | 3.83e-03 | 6.58e-05 |
| p(                         | $GE_2GE_1$                      | 5           | 1.34e-04             | 3.05e-04 | 3.27e-06 |
| 36                         | $GB_2GB_1$                      | 5           | 1.01001              | 2.77e-04 | 1.38e-05 |
| 2                          | $EC_2EC_1$                      | 6           | 7.66e-05             | 3.35e-04 | 8.27e-06 |
| -2                         | $GF_2GF_1$                      | 7           | 5.08e-06             | 2.50e-05 | 9.96e-07 |
| -01                        | $GB_2GB_1$                      | 7           | 5.04e-06             | 2.52e-05 | 9.32e-07 |
| •                          | $EC_2EC_1$                      | 8           | 5.15e-06             | 2.59e-05 | 1.19e-06 |
| 8                          | $GF_2GF_1$                      | 9           | 1.57e-05             | 1.17e-06 | 3.03e-07 |
| =<br>2                     | $GB_2GB_1$                      | 9           | 1.55e-05             | 1.23e-06 | 3.28e-07 |
| h                          | $EC_2EC_1$                      | 10          | 1.62e-05             | 9.85e-07 | 3.28e-07 |
|                            | CE <sub>2</sub> CE <sub>4</sub> | 3           | 9.630-04             | 4.06e-04 | 3 780-04 |
| tts                        | GB <sub>2</sub> GB <sub>1</sub> | 3           | 1.320-04             | 6.110-04 | 1.00e-04 |
| nic                        | $EC_2EC_1$                      | 4           | 1.52e-04<br>4.03e-04 | 1.82e-04 | 4.000-04 |
| p(                         | $GE_2GE_1$                      | 5           | 4.86e-06             | 4.11e-06 | 1.20e-07 |
| 71                         | $GB_{2}GB_{1}$                  | 5           | 4.000-00<br>4.12e-06 | 3.42e-06 | 3 39e-07 |
| 4                          | $EC_2EC_1$                      | 6           | 1.12c-00<br>1.34e-06 | 4.30e-06 | 1.10e-07 |
| , 2                        | $GE_2GE_1$                      | 7           | 7 10e-08             | 5.31e-08 | 3.88e-10 |
| -0-                        | $GB_2GB_1$                      | 7           | 6.95e-08             | 5.43e-08 | 5.25e-10 |
| · ·                        | $EC_2EC_1$                      | 8           | 5.18e-08             | 5.15e-08 | 1.67e-10 |
| : 4                        | $GF_2GF_1$                      | 9           | 8.22e-10             | 9.95e-11 | 7.58e-12 |
|                            | $GB_2GB_1$                      | 9           | 6.06e-10             | 6.65e-11 | 2.09e-11 |
| Ч                          | $EC_2EC_1$                      | 10          | 6.62e-10             | 4.85e-10 | 1.10e-11 |
|                            | CF-CF.                          | 3           | 1 120 04             | 6 300 05 | 4 780 05 |
| tts                        | $GB_2GP_1$                      | 3           | 2.27e-05             | 6.13e-05 | 4.91e-05 |
| in                         | $EC_2EC_1$                      | 4           | 5.56e-05             | 3.69e-06 | 2.81e-07 |
| p(                         | $GF_2GF_1$                      | 5           | 2.50e-07             | 6.00e-08 | 5.90e-09 |
| 42                         | $GB_2GB_1$                      | 5           | 2.27e-07             | 4.01e-08 | 9.14e-09 |
| 6                          | $EC_2EC_1$                      | 6           | 2.93e-08             | 5.99e-08 | 1.76e-09 |
| - 2                        | $GF_2GF_1$                      | 7           | 7.51e-10             | 1.91e-10 | 3.63e-12 |
| -01                        | $GB_2GB_1$                      | 7           | 8.50e-10             | 1.88e-10 | 6.02e-11 |
| •                          | $EC_2EC_1$                      | 8           | 3.95e-10             | 1.82e-10 | 8.24e-11 |
| = 2                        | $GF_2GF_1$                      | 9           | 9.16e-10             | 4.12e-10 | 1.57e-11 |
| =<br>7                     | $GB_2GB_1$                      | 9           | 9.70e-10             | 1.59e-10 | 6.85e-12 |
| 4                          | $EC_2EC_1$                      | 10          | 3.97e-10             | 1.57e-10 | 1.34e-10 |
|                            | GE <sub>0</sub> GE <sub>1</sub> | 3           | 1 17e-05             | 8 81e-06 | 6.01e-06 |
| $\mathbf{nt}_{\mathbf{t}}$ | $GB_2GB_1$                      | 3           | 5.79e-06             | 6.70e-06 | 6.09e-06 |
| ioi                        | $EC_2EC_1$                      | 4           | 7.26e-06             | 7.76e-07 | 1.70e-08 |
| с р                        | $GF_2GF_1$                      | 5           | 1.49e-08             | 1.85e-09 | 6.59e-10 |
| 385                        | $GB_2GB_1$                      | $\tilde{5}$ | 1.37e-08             | 1.10e-09 | 2.17e-10 |
| 15                         | $EC_2EC_1$                      | 6           | 5.10e-10             | 1.09e-09 | 1.67e-10 |
| , -2                       | $GF_2GF_1$                      | $\tilde{7}$ | 3.98e-10             | 1.28e-10 | 3.38e-10 |
| _0                         | $GB_2GB_1$                      | 7           | 9.65e-11             | 3.56e-10 | 3.04e-10 |
| . 1                        | $EC_2EC_1$                      | 8           | 3.32e-10             | 3.25e-10 | 3.30e-10 |
| -                          | $GF_2GF_1$                      | 9           | 3.68e-09             | 2.43e-09 | 6.34e-11 |
| 11                         | $GB_2GB_1$                      | 9           | 3.95e-10             | 1.57e-09 | 1.77e-10 |
| h                          | $EC_2EC_1$                      | 10          | 2.76e-09             | 7.96e-10 | 4.53e-10 |

Table 4: Numerical results for Test problem 2, constant stepsize.

|            | Main                            |        | 1                    | Error                |                      |
|------------|---------------------------------|--------|----------------------|----------------------|----------------------|
|            | Scheme                          | Order  | Method1              | Method2              | Method3              |
| so<br>v    | $GF_2GF_1$                      | 3      | 5.20e-05             | 6.97e-05             | 1.42e-05             |
| int        | $GB_2GB_1$                      | 3      | 3.23e-05             | 3.63e-05             | 6.13e-06             |
| iod        | $EC_2EC_1$                      | 4      | 1.10e-04             | 9.47e-05             | 3.71e-06             |
| 5          | $GF_2GF_1$                      | 5      | 7.00e-06             | 7.29e-06             | 7.35e-07             |
| 12         | $GB_2GB_1$                      | 5      | 6.50e-06             | 6.83e-06             | 6.34e-07             |
| <b>6</b>   | $EC_2EC_1$                      | 6<br>7 | 9.29e-06             | 8.91e-06             | 7.17e-07             |
| _ 0        | $GF_2GF_1$                      | 7      | 1.10e-06             | 1.17e-06             | 5.32e-08             |
| . 1        | $GD_2GD_1$                      | 6      | 1.11e-00<br>1.36c.06 | 1.12e-00<br>1.35c.06 | 5.57e-08             |
| $\infty$   | $CE_2EC_1$                      | 0      | 2.39e-07             | 2.40e-07             | 0.95e-08             |
| II         | $GB_2GP_1$<br>$GB_2GB_1$        | 9      | 2.33e-07<br>2.34e-07 | 2.40e-07<br>2.35e-07 | 1.11e-08             |
| Ч          | $EC_2EC_1$                      | 10     | 2.68e-07             | 2.68e-07             | 1.24e-08             |
|            | CF2CF1                          | 3      | 1.54e-06             | 7.11e-06             | 1.75e-06             |
| nts        | $GB_2GP_1$<br>$GB_2GB_1$        | 3      | 3 23e-05             | 2.57e-06             | 1.75e-00<br>1.23e-06 |
| oin        | $EC_2EC_1$                      | 4      | 1.31e-05             | 9.19e-06             | 2.51e-07             |
| pe         | $GF_2GF_1$                      | 5      | 1.92e-07             | 2.27e-07             | 1.80e-08             |
| 50         | $GB_2GB_1$                      | 5      | 1.77e-07             | 2.15e-07             | 1.20e-08             |
| , 2        | $EC_2EC_1$                      | 6      | 3.31e-07             | 2.85e-07             | 1.58e-08             |
| -2         | $GF_2GF_1$                      | 7      | 1.31e-08             | 1.36e-08             | 4.06e-10             |
| 10         | $GB_2GB_1$                      | 7      | 1.25e-08             | 1.30e-08             | 4.62e-10             |
| ÷          | $EC_2EC_1$                      | 8      | 1.68e-08             | 1.59e-08             | 5.54e-10             |
|            | $GF_2GF_1$                      | 9      | 1.10e-09             | 1.12e-09             | 3.52e-11             |
| - <i>u</i> | $GB_2GB_1$                      | 9      | 1.07e-09             | 1.09e-09             | $3.53e{-}11$         |
|            | $EC_2EC_1$                      | 10     | 1.29e-09             | 1.26e-09             | 3.96e-11             |
| ŝ          | $GF_2GF_1$                      | 3      | 2.75e-06             | 6.92e-07             | 2.12e-07             |
| int        | $GB_2GB_1$                      | 3      | 3.40e-06             | 1.38e-07             | 1.79e-07             |
| od         | $EC_2EC_1$                      | 4      | 1.56e-06             | 8.35e-07             | 1.61e-08             |
| 0          | $GF_2GF_1$                      | 5      | 2.54e-09             | 5.54e-09             | 3.70e-10             |
| 50         | $GB_2GB_1$                      | 5      | 2.26e-09             | 5.34e-09             | 1.58e-10             |
| <b>6</b> 0 | CE CE                           | 0<br>7 | 1.03e-08             | 7.19e-09<br>1.02e 10 | 2.70e-10<br>6.75c 12 |
| _ 0        | $GF_2GF_1$                      | 7      | 9.15e-11<br>8.50a 11 | 1.03e-10             | 0.75e-12             |
| . 1        | $EC_2EC_1$                      | 8      | 0.59e-11<br>1.46e-10 | 9.82e-11<br>1.21e-10 | $5.62e^{-12}$        |
| 2          | $GE_2GE_1$                      | 9      | 1.40c-10<br>1.08e-11 | 7.93e-12             | 1.02e-12             |
|            | $GB_2GB_1$                      | 9      | 5.48e-12             | 6.21e-12             | 1.92e-11             |
| Ч          | $EC_2EC_1$                      | 10     | 8.68e-12             | 5.87e-12             | 1.79e-11             |
| w .        | GF <sub>2</sub> GF <sub>1</sub> | 3      | 9.03e-07             | 6.97e-08             | 2.58e-08             |
| nti        | $GB_2GB_1$                      | 3      | 9.85e-07             | 7.78e-09             | 2.37e-08             |
| ioc        | $EC_2EC_1$                      | 4      | 1.89e-07             | 7.82e-08             | 1.01e-09             |
| 0 I        | $GF_2GF_1$                      | 5      | 2.11e-10             | 1.24e-10             | 7.95e-12             |
| 00         | $\mathrm{GB}_2\mathrm{GB}_1$    | 5      | 2.22e-10             | 1.22e-10             | 5.75e-12             |
| , 1        | $\mathrm{EC}_2\mathrm{EC}_1$    | 6      | 3.11e-10             | 1.66e-10             | 4.63e-12             |
| -2         | $GF_2GF_1$                      | 7      | 3.93e-12             | 1.67e-12             | 3.48e-12             |
| 10         | $GB_2GB_1$                      | 7      | 3.51e-12             | 2.29e-12             | 4.38e-12             |
| ÷          | $EC_2EC_1$                      | 8      | 5.28e-12             | 2.29e-12             | 2.72e-12             |
|            | $GF_2GF_1$                      | 9      | 3.60e-11             | 2.16e-11             | 1.88e-12             |
| - <i>u</i> | $GB_2GB_1$                      | 9      | 5.38e-12             | 1.41e-11             | 2.13e-12             |
| -          | $EC_2EC_1$                      | 10     | 1.38e-11             | 1.18e-11             | 3.63e-12             |

Table 5: Numerical results for Test problem 3, constant stepsize.

| Main                         |       | Metho    | d1   | Metho    | d3   |
|------------------------------|-------|----------|------|----------|------|
| Scheme                       | Order | Error    | Mesh | Error    | Mesh |
| $GF_2GF_1$                   | 3     | 5.35e-06 | 751  | 3.03e-07 | 593  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 3     | 3.92e-06 | 898  | 1.88e-07 | 817  |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 4     | 4.91e-07 | 1038 | 8.10e-09 | 809  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 5     | 1.69e-08 | 407  | 1.61e-08 | 291  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 5     | 2.94e-08 | 407  | 1.49e-08 | 331  |
| $EC_2EC_1$                   | 6     | 3.36e-08 | 434  | 4.40e-09 | 321  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 7     | 1.11e-09 | 288  | 4.93e-10 | 217  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 7     | 7.49e-10 | 288  | 1.54e-09 | 193  |
| $EC_2EC_1$                   | 8     | 3.20e-09 | 288  | 5.48e-10 | 217  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 9     | 3.45e-10 | 223  | 5.39e-11 | 183  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 9     | 2.74e-10 | 223  | 7.83e-11 | 183  |
| $EC_2EC_1$                   | 10    | 5.88e-10 | 223  | 8.99e-11 | 183  |

Table 6: Numerical results for Test problem 1 with y(0) = 1, variable stepsize.

Table 7: Numerical results for Test problem 1 with y(0) = 2, variable stepsize.

| Main                         |       | Method1  |      | Metho      | d3   |
|------------------------------|-------|----------|------|------------|------|
| Scheme                       | Order | Error    | Mesh | Error      | Mesh |
| $GF_2GF_1$                   | 3     | 9.36e-06 | 240  | 7.84e-07   | 169  |
| $GB_2GB_1$                   | 3     | 6.89e-06 | 275  | 5.62 e- 07 | 209  |
| $EC_2EC_1$                   | 4     | 1.38e-06 | 268  | 1.75e-08   | 177  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 5     | 1.25e-08 | 137  | 3.93e-08   | 101  |
| $GB_2GB_1$                   | 5     | 5.35e-08 | 137  | 4.34e-08   | 121  |
| $EC_2EC_1$                   | 6     | 1.20e-07 | 146  | 1.64e-08   | 111  |
| $GF_2GF_1$                   | 7     | 1.04e-08 | 112  | 4.31e-09   | 97   |
| $GB_2GB_1$                   | 7     | 7.13e-09 | 112  | 6.83e-09   | 85   |
| $EC_2EC_1$                   | 8     | 1.47e-08 | 112  | 2.74e-09   | 97   |
| $GF_2GF_1$                   | 9     | 1.82e-09 | 106  | 1.66e-09   | 85   |
| $GB_2GB_1$                   | 9     | 1.38e-09 | 106  | 3.18e-09   | 85   |
| $EC_2EC_1$                   | 10    | 2.23e-09 | 106  | 2.32e-09   | 85   |

| Main                         |       | Method1  |      | Metho    | d3   |
|------------------------------|-------|----------|------|----------|------|
| Scheme                       | Order | Error    | Mesh | Error    | Mesh |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 3     | 9.09e-05 | 1311 | 2.88e-05 | 1113 |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 3     | 1.70e-04 | 1206 | 2.88e-05 | 1113 |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 4     | 1.98e-05 | 1199 | 2.94e-06 | 761  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 5     | 1.52e-06 | 542  | 4.27e-07 | 421  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 5     | 1.29e-06 | 560  | 2.52e-06 | 351  |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 6     | 8.14e-07 | 542  | 5.56e-07 | 371  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 7     | 1.08e-06 | 343  | 1.10e-07 | 253  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 7     | 1.04e-06 | 343  | 9.34e-08 | 265  |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 8     | 7.58e-06 | 343  | 1.80e-07 | 253  |
| $\mathrm{GF}_2\mathrm{GF}_1$ | 9     | 1.45e-07 | 275  | 1.22e-06 | 197  |
| $\mathrm{GB}_2\mathrm{GB}_1$ | 9     | 1.56e-07 | 275  | 2.16e-06 | 197  |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 10    | 3.42e-07 | 275  | 1.09e-06 | 197  |

Table 8: Numerical results for Test problem 2, variable stepsize.

|                              |       | Method1  |      | Metho      | d3   |
|------------------------------|-------|----------|------|------------|------|
| Method                       | Order | Error    | Mesh | Error      | Mesh |
| $GF_2GF_1$                   | 3     | 2.57e-06 | 233  | 2.25e-07   | 193  |
| $GB_2GB_1$                   | 3     | 2.68e-06 | 247  | 3.58e-07   | 153  |
| $EC_2EC_1$                   | 4     | 7.42e-07 | 240  | 1.72e-08   | 185  |
| $GF_2GF_1$                   | 5     | 2.65e-08 | 119  | 7.94e-09   | 101  |
| $GB_2GB_1$                   | 5     | 2.00e-08 | 119  | 5.62 e- 09 | 101  |
| $EC_2EC_1$                   | 6     | 6.55e-08 | 128  | 6.15e-09   | 101  |
| $GF_2GF_1$                   | 7     | 1.60e-08 | 90   | 1.74e-09   | 73   |
| $GB_2GB_1$                   | 7     | 1.43e-08 | 90   | 2.07e-09   | 73   |
| $EC_2EC_1$                   | 8     | 1.84e-08 | 101  | 2.13e-09   | 85   |
| $GF_2GF_1$                   | 9     | 1.18e-08 | 80   | 2.67e-09   | 71   |
| $GB_2GB_1$                   | 9     | 1.10e-08 | 80   | 2.77e-09   | 71   |
| $\mathrm{EC}_2\mathrm{EC}_1$ | 10    | 1.32e-08 | 80   | 2.72e-09   | 71   |

Table 9: Numerical results for Test problem 3, variable stepsize.

has been solved with initial conditions y(0) = 1 and y'(0) = -1 or y(0) = 2 and y'(0) = -1. The roots of  $z^2 + z = 0$  are -1 and 0 and, therefore, the exact solution is

$$y_e(t) = \mathrm{e}^{-t} + c_2,$$

where  $c_2 = y(0) - 1$ . Tables 3, 6 and 7 are devoted to this example. Tables 3 and 6 solve the problem with the first choice of initial conditions while Table 7 makes use of the second choice.

Even if the numerical solution is monotone decreasing, it might tend to a negative value when  $c_2 = 0$ . For this reason, in Table 3 we also indicate when the numerical solution eventually becomes negative. With constant stepsize we have not observed differences between the two problems (for this reason we have discarded the table associated to the second choice of initial conditions). Vice versa, with variable stepsize, the problem with the second choice of initial conditions has required a much lower number of points.

Problem 2. The second linear problem,

$$y''(t) - \cos t \ y'(t) + \sin t \ y(t) = 0, \quad t \in [0, 6\pi],$$

has initial conditions y(0) = 1 and y'(0) = 1. The exact solution,

$$y_e(t) = \mathrm{e}^{\sin t},$$

has an oscillating solution with period  $2\pi$ .

Problem 3. The nonlinear problem

$$(y(t) + 1) y''(t) - 3(y'(t))^2 = 0, \qquad t \in [1, 10],$$

has initial conditions y(1) = 0 and  $y'(1) = -\frac{1}{2}$ . The exact solution is

$$y_e(t) = \frac{1}{\sqrt{t}} - 1.$$

From all these examples we obtain that the higher order methods compute a more accurate solution also when a large stepsize is used. On the contrary, due to the large size of the systems, with the smallest constant stepsize considered it is not always possible to achieve the best accuracy (see the last block of Tables 3, 4 and 5). Method 2 gives always the worst results. Moreover, its solution for the first problem always gives a negative solution when the stepsize  $h = 8 \cdot 10^{-2}$ . Anyway, the main drawback of all these methods seems to be just that they do not preserve the sign of the solution.

#### 5 Conclusions

In this paper we propose to solve second order ordinary differential equations with initial conditions approximating each derivative by means of a set of finite difference schemes. We have derived several methods depending on the choice of the main scheme and the additional formulae. Concerning this last aspect, we have obtained the best results by considering the first derivative at the extreme points (the left one is a known value) inside each block of unknowns. Vice versa we have not observed differences among the possible choices of the main scheme. The choice of the Generalized Forward methods for the first derivative gives larger stability domains and could be more convenient for the most difficult problems.

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