

ORTHONORMAL FRAMES ON SPACE CURVES

①

Right-handed orthonormal frame $(\underline{e}_1(\xi), \underline{e}_2(\xi), \underline{e}_3(\xi))$
on space curve $\underline{r}(\xi)$.

$$|\underline{e}_i(\xi)| = 1 \Rightarrow \underline{e}_i(\xi) \cdot \underline{e}_i'(\xi) = 0 \text{ so } \underline{e}_i'(\xi) \perp \underline{e}_i(\xi)$$

Regard parameter ξ as 'time':

$$\underline{e}_i'(\xi) = \underline{\omega}(\xi) \times \underline{e}_i(\xi), \quad \underline{\omega}(\xi) = \text{frame angular velocity}$$

Can express $\underline{\omega}$ in terms of $(\underline{e}_1, \underline{e}_2, \underline{e}_3)$ as

$$\underline{\omega} = \omega_1 \underline{e}_1 + \omega_2 \underline{e}_2 + \omega_3 \underline{e}_3$$

Frenet frame: tangent, principal normal, binormal
 $(\underline{t}, \underline{p}, \underline{b})$ is more familiar.

$$\underline{t} = \frac{\underline{r}'}{|\underline{r}'|} : \text{direction of motion along } \underline{r}(\xi)$$

$$\underline{p} = \frac{\underline{r}' \times \underline{r}''}{|\underline{r}' \times \underline{r}''|} \times \underline{t} : \text{points to center of curvature}$$

$$\underline{b} = \frac{\underline{r}' \times \underline{r}''}{|\underline{r}' \times \underline{r}''|} : \text{normal to osculating plane}$$

Define parametric speed $\sigma = |\dot{\underline{r}}|$,
curvature $K = \frac{|\dot{\underline{r}} \times \ddot{\underline{r}}|}{|\dot{\underline{r}}|^3}$, torsion $\tau = \frac{(\dot{\underline{r}} \times \ddot{\underline{r}}) \cdot \dddot{\underline{r}}}{|\dot{\underline{r}} \times \ddot{\underline{r}}|^2}$ (2)

Frenet frame angular velocity:

$$\underline{\omega} = \sigma(\tau \underline{t} + K \underline{b}) = \text{"Darboux vector"}$$

NOTE: $\underline{\omega}$ has no component in direction of \underline{p} ,
ie, no instantaneous rotation of $\underline{b}, \underline{t}$ about \underline{p} .

$\Rightarrow (\underline{t}, \underline{p}, \underline{b})$ is "rotation-minimizing" w.r.t. \underline{p}

Defects of Frenet frame:

1. $(\underline{t}, \underline{p}, \underline{b})$ do not depend rationally on parameter ξ
2. \underline{p} & \underline{b} usually suffer sudden reversals at inflection points, where $K=0$.
3. For many applications, prefer frame that is rotation-minimizing w.r.t. \underline{t} rather than \underline{p}
(robotics, animation, 5-axis CNC machining, swept surface constructions, etc.)

Rotation-minimizing "adapted" frame $(\underline{t}, \underline{u}, \underline{v})$ (3)
 consists of tangent \underline{t} and normal-plane vectors $\underline{u}, \underline{v}$ that exhibit no rotation about \underline{t} .

Euler-Rodrigues frame (ERF) = a rational
 adapted frame defined on any spatial PH curve:

$$(\underline{e}_1(\xi), \underline{e}_2(\xi), \underline{e}_3(\xi)) = \frac{(A(\xi)\underline{i}A^*(\xi), A(\xi)\underline{j}A^*(\xi), A(\xi)\underline{k}A^*(\xi))}{|A(\xi)|^2}$$

$\underline{e}_1(\xi)$ = tangent; $\underline{e}_2(\xi)$ & $\underline{e}_3(\xi)$ span normal plane.
 All rationally dependent on ξ .

If $A(\xi) = u(\xi)\underline{i} + v(\xi)\underline{j} + p(\xi)\underline{k} + q(\xi)\underline{l}$ and

$$\sigma(\xi) = |A(\xi)|^2 = u^2(\xi) + v^2(\xi) + p^2(\xi) + q^2(\xi),$$

the ERF angular velocity $\underline{\omega} = \omega_1 \underline{e}_1 + \omega_2 \underline{e}_2 + \omega_3 \underline{e}_3$

has components

$$\omega_1 = \frac{2(uv' - u'v - pq' + p'q)}{\sigma}$$

$$\omega_2 = \frac{2(up' - u'p + vq' - v'q)}{\sigma}$$

$$\omega_3 = \frac{2(uq' - u'q - vp' + v'p)}{\sigma}$$

NOTE: $\sigma' = 2 \text{scal}(A'A^*)$, $\sigma \underline{\omega} = 2 \text{vect}(A'A^*)$ (4)

$$\Rightarrow \sigma'^2 + \sigma^2 |\underline{\omega}|^2 = 4|A|^2 |A'|^2$$

ERF is not rotation-minimizing w.r.t. $\underline{e}_1 = \underline{t}$, since $\omega_1 \neq 0$.

If $\rho(\xi)$ admits a rational rotation-minimizing frame $(\underline{t}, \underline{u}, \underline{v})$ it must be obtainable from the ERF $(\underline{t}, \underline{e}_2, \underline{e}_3)$ by a rational normal-plane rotation:

$$\begin{bmatrix} \underline{u}(\xi) \\ \underline{v}(\xi) \end{bmatrix} = \frac{1}{a^2(\xi) + b^2(\xi)} \begin{bmatrix} a^2(\xi) - b^2(\xi) & -2a(\xi)b(\xi) \\ 2a(\xi)b(\xi) & a^2(\xi) - b^2(\xi) \end{bmatrix} \begin{bmatrix} \underline{e}_2(\xi) \\ \underline{e}_3(\xi) \end{bmatrix}$$

where $a(\xi), b(\xi) =$ polynomials with $\text{gcd}(a, b) = 1$.

Corresponds to normal-plane rotation by angle

$$\theta(\xi) = -2 \tan^{-1} \frac{b(\xi)}{a(\xi)}$$

which induces angular velocity component

$$\sigma' = \frac{2(a'b - ab')}{a^2 + b^2} \quad \text{in } \underline{e}_1 = \underline{t} \text{ direction}$$

For a rational rotation-minimizing frame (RRMF) curve, θ' must exactly cancel ω_1 component of ERF angular velocity.

$\mathcal{P}'(\xi) = A(\xi) i A^*(\xi)$ with $A = u + v\underline{i} + p\underline{j} + q\underline{k}$ defines an RRMF curve \Leftrightarrow there exist polynomials $a(\xi), b(\xi)$ with $\gcd(a, b) = 1$ such that:

$$\frac{uw' - u'w - pq' + p'q}{u^2 + v^2 + p^2 + q^2} = \frac{ab' - a'b}{a^2 + b^2}$$

* There are no non-trivial (i.e., non-planar) cubic RRMF curves.

* There exist non-trivial quintic RRMF curves (a proper subset of all spatial PH quintics).

